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(71) Applicant: NTT Mobile Communications Network
Inc.
Tokyo 100-8150 (JP)

(72) Inventor: Ryo, Yamaguchi,
NTT Mobile Communicat.Network Inc.
Chiyoda-ku, Tokyo 100-8150 (JP)

(74) Representative: Midgley, Jonathan Lee
Marks & Clerk
57-60 Lincoln's Inn Fields
GB-London WC2A 3LS (GB)

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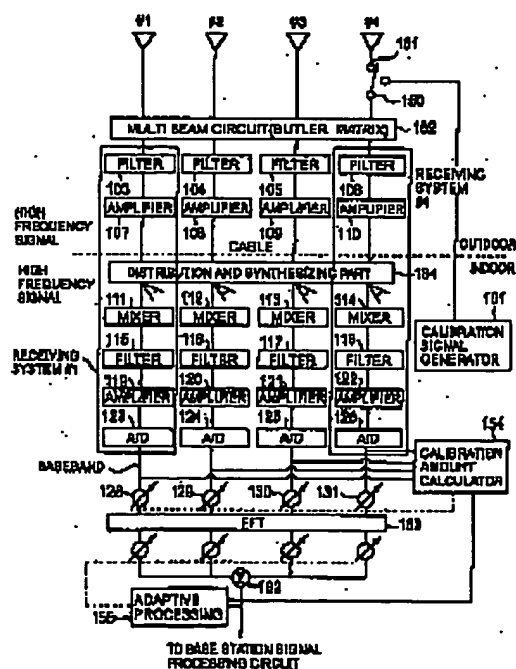
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(54) Calibration for an adaptive array antenna

(57) An adaptive array antenna comprising a plurality of array antennas including a plurality of antenna elements which are spaced at intervals at which a large correlation is exhibited, said array antennas being spaced at intervals at which the correlation is negligible, wherein diversity effects such as fading compensation

are produced, interference waves coming from the same direction are eliminated, the gain is augmented by main beam tracking, and one or more calibration signal coupling parts and multi-beam synthesizing circuit are provided so as to remove individual variations in calibration signals and to perform highly reliable calibration.

FIG.4



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Description

TECHNICAL FIELD

[0001] The present invention relates to an adaptive array antenna and a method for calculating a calibration amount of a receiving system of the adaptive array antenna and a method for calibration.

BACKGROUND ART

[0002] Generally, the adaptive array antenna is used for beam control of array antennas. There are two kinds of algorithms for the beam control, which are an interference suppression tracking type and a maximum gain tracking type. In the interference suppression tracking type, tracking is performed having a null point to interference waves and having strong directivity to desired waves. In the maximum gain tracking type, tracking is performed such that the receiving level of the antenna is maximized. In each of the types, a mobile station can be tracked by a main beam. At the current time, the spacing between elements of the array antenna is usually $\lambda/2$ as shown in Fig. 12. The reason for this is that a grating lobe may occur when the spacing is more than $\lambda/2$ as shown in Fig. 13. The grating lobe may increase interference since the main lobe can be distracted to an unnecessary direction. Although the width of the beam narrows, gain increase by this is not obtained.

[0003] Because the spacing between elements of the array antenna shown in Fig. 12 is narrow, the correlation between the elements is very high. Therefore, when the receiving level deteriorates due to fading, the deterioration influences all elements 1-8 which are included in the array antenna so that the deterioration can not be compensated for. Especially, the phenomenon is remarkable for a small sized array antenna which has about 4 elements. In addition, in the interference suppression tracking type algorithm, when there are interference waves coming from near the direction of desired waves, the interference suppression capability deteriorates remarkably since the interference waves exist in the main lobe.

[0004] That is, in the narrow element spacing adaptive signal processing, correlation of envelope and signal between elements is extremely strong and the phase deviation is less than a wave length. In the interference suppression tracking type algorithm, wait (phase and amplitude) of each antenna element is obtained such that the interference waves cancel each other out and the desired waves do not cancel each other out. Interference waves which come from a direction different enough from the desired waves are input into the antenna as a signal having strong envelope and signal correlation like the desired waves. However, since the arriving angle is different, the phase difference of the interference waves between elements is different from the phase difference of the desired waves. As a result, the

desired waves are not necessarily in opposite phase for a wait in which the interference waves are in opposite phase. In many cases, the desired waves operate as in phase. On the other hand, when the arriving direction of the interference waves is close to the desired waves, the amount of phase shift of the desired waves and the interference waves is almost the same. Therefore, the attempt to cancel the interference waves may result in cancelling the desired waves so that the interference suppression capability deteriorates.

[0005] On the other hand, since a diversity antenna is designed such that the correlation between elements becomes small, the spacing between elements 21-28 is large as shown in Fig. 14. Since the correlation is small, when the receiving level of an element declines, the receiving level of another element may be high. Generally, a maximal ratio combining (MRC) algorithm is applied. According to the maximal ratio combining algorithm, receiving waves of each of the antenna elements 21-28 are synthesized after assigning weights of envelope level of the receiving waves after placing the receiving waves in phase. According to this algorithm, the concept of beam control is not applied because the spacing between elements is large, thus, many ripples exist in the envelope which is the beam of each element. Therefore, tracking is not performed since too many main beams exist. Thus, the gain increase by narrowing the beam can not be expected. According to the algorithm, when there are the interference waves, the influence is directly exerted. Because, as mentioned above, in the synthesizing method, amplitude and phase are controlled such that signals of all elements can be received at maximum gain, and the interference waves and the desired waves are treated without distinction. Accordingly, the method of the maximum ratio synthesizing diversity shown in Fig. 14 is effective for improving receiving characteristics of a desired station that has deterioration due to fading. However, the method does not contribute to improved interference characteristics.

[0006] As mentioned above, the narrow element spacing adaptive array antenna of the interference suppression tracking type is effective in suppressing interference waves other than from main beam. However, the antenna has no effect for suppressing interference waves in the main beam and fading. On the other hand, although the diversity antenna which has the wide element spacing can compensate for deterioration of characteristics of the desired waves due to fading, the diversity antenna has no effect pertaining to interference waves.

[0007] In addition, there are two more combinations of antenna placements (narrow element spacing, wide element spacing) and algorithms (maximum ratio synthesizing, interference suppression). First, the combination is the maximum gain tracking type which uses the narrow element spacing as shown in Fig. 15 and the maximum ratio synthesizing algorithm. Second, the combination is the interference suppression type which

uses the wide element spacing as shown in Fig.16. In the method shown in Fig.16, the antenna is set for diversity configuration and the algorithm is the interference suppression type. According to the method, capability of interference wave suppression is kept as the basic characteristic of the algorithm. In addition, fading can be compensated for since the correlation between elements is small in the diversity configuration. Especially, the characteristic is remarkable when the angle of spreading of arriving waves is large. A wait (phase and amplitude) can be determined such that many coming element waves of the interference waves are statistically canceled out because phase differences due to the arriving angle are different. Therefore, even if the arriving angles are the same, a wait can be generated such that the desired waves become in-phase and the interference waves become opposite phase.

[0008] However, according to the combination method of the maximum gain tracking type which uses the narrow element spacing shown in Fig.15 and the maximum ratio synthesizing algorithm, high gain can be obtained and the desired waves can be tracked with an antenna similar to the adaptive array antenna shown in Fig.12. However, the method has no effect on interference waves and fading. In addition, according to the combination method using the wide element spacing and the interference suppression type shown in Fig. 16, gain increase can not be obtained because the wide-ness of the element spacing prevents tracking by the main beam.

[0009] One of the objects of the invention of the parent application, EP-A-1014485, is to solve the above-mentioned problems.

The object is to provide an adaptive array antenna which has diversity effects such as fading compensation or the like, eliminates the interference waves from the same direction and increases gain by main beam tracking.

[0010] In order to obtain effects which are diversity effects such as fading compensation or the like, removing interference waves from the same direction and increasing gain by main beam tracking, the adaptive array antenna needs to be accurately calibrated. In the following, the calibration will be described.

[0011] In the adaptive array antenna, it is necessary that amplitude ratio and phase difference in a high frequency band occurring between element antennas are maintained to baseband on which signal processing is performed. Generally, since a cable, an amplifier, a filter, a mixer, a converter and the like have different electronic characteristics, it is difficult to equate the amplitudes and phases of all the elements. (In the following, the electronic difference between elements will be called "individual variation".) In addition, it is practically impossible to equate the amplitudes and phases since there are differences due to temperature in addition to the general differences.

Therefore, as shown in Fig.17, it is conceivable to measure the amplitude ratio and the phase difference be-

tween the elements by providing the same calibration signals to each antenna and correct the amplitude ratio and the phase difference beforehand based on the measurement in order to keep the amplitude ratio and the phase difference constant within a fixed period.

[0012] The calibration signal can be realized by inserting the signal into a frame format at each channel during constant time intervals of one minute or ten minutes or the like. A calibration signal input terminal may be described as a switch type shown in Fig.18A in the following description. In addition, the terminal may be a type that connects to an antenna cable or the like electromagnetically as shown in Fig.18B. In the switch type, communication is interrupted during the switching.

On the other hand, the type using an electromagnet connection has the effect that there is no such interruption. In the Figs.18A, 18B, the array antenna is connected to the terminals a and b and the calibration signal is applied to the terminal c.

[0013] The part where the calibration signal is applied is called a calibration signal coupling part, which includes the calibration signal input terminals of the switch type and the electromagnetically connecting type.

[0014] Fig.17 shows the array antenna which includes antenna elements #1-#4. Signals received by each of the antenna elements are applied to a distribution and synthesizing part 134 via filters 109-108 and high frequency amplifiers 107-110. In the distribution and synthesizing part 134, the signal received by the antenna is distributed to channels. Therefore, the signals after the distribution and synthesizing part 134 are transmitted to a plurality of channels. However, one channel in the plurality of channels is shown in Fig.17. The received signals distributed by the distribution and synthesizing part 134 are added at a signal adder 132 via mixers 111-114, filters 115-118, intermediate frequency amplifiers 119-122, A/D converters (analog digital converters) 123-126 and waits 128-131. An adaptive signal processing device 133 controls amplitude and phase of the waits 128-131. As a result, the received signals are transmitted to a base station signal processing circuit.

[0015] The output from a calibration signal generator 101 is split in four by a signal splitter 102 and at the same time the calibration signals are applied to filters 103-106 via cables 176-179 and calibration signal input terminals 166-169 in the antenna elements #1-#4. These signals are transmitted to the base station signal processing circuit in the same way as received signals. At the time, output signals from the A/D converters 123-126 are applied to a calibration amount calculator 127. The calibration amount calculator 127 compares the amplitude and the phase of each A/D converters 123-126 with each other and calculates calibration amount for equalizing amplitude change and phase change between the antenna elements #1-#4 and the signal adder 132 in the receiving systems. The receiving system here is a system which includes a series of circuits for receiving connected to the output of the antenna. That is, the receiv-

ing system includes the filter, the high frequency amplifier, the mixer, the filter, the intermediate frequency amplifier and the AD converter. Four receiving systems are included in Fig. 17. The calibration amount is transmitted to the adaptive signal processing device 133. The adaptive signal processing device 133 stores the calibration amount in a calibration table (which is not shown in the figure). When the adaptive signal processing device 133 performs adaptive signal processing, the adaptive signal processing device 133 controls the waits 128-131 by subtracting the calibration amount.

[0016] However, the calibration signals, provided to antennas, which are regarded to be the same, have the individual variations. In Fig. 17, the calibration signal generator 101 needs to divide the output signal into the same number of signals as there are elements of the array antenna and needs to transmit the calibration signals to the calibration signal coupling part via the cables 175-178. Since the cables 175-178 and the calibration terminals have individual variations (cable characteristics and cable lengths and the like), phase differences occur in the calibration signals. As a result, there is a problem in that a calibration error occurs.

[0017] Thus, the object of the present invention is to realize reliable calibration by eliminating effects based on the individual variations to the calibration signal.

[0018] The present invention has the following means as means for achieving the object.

[0019] The invention as claimed in claim 1 is an adaptive array antenna characterized in that said adaptive array antenna comprises: an array antenna having a plurality of antenna elements; a multi-beam synthesizing circuit for synthesizing multiple beams; a calibration signal coupling part, provided between said multi-beam synthesizing circuit and said antenna element, for inputting a calibration signal; a calibration signal generator; a calibration amount calculator; wherein said calibration signal generator applies a calibration signal output to said calibration signal coupling part, said calibration amount calculator calculating a calibration amount of each of receiving systems from baseband signals of said receiving systems connected to the outputs of said multi-beam synthesizing circuit and performing calibration of said receiving systems.

[0020] According to the invention as claimed in claim 1, a calibration signal is applied to the calibration signal coupling part which is provided between the multi-beam synthesizing circuit and an antenna element. And, the calibration amount is calculated for each receiving system from a baseband signal of the receiving system which is connected to the output of the multi-beam synthesizing circuit and calibration is performed on the receiving systems. Accordingly, individual variations between the calibration signals are eliminated such that reliable calibration can be realized.

[0021] The invention as claimed in claim 2 is an adaptive array antenna comprising: an array antenna having a plurality of antenna elements; a multi-beam synthesizing

ing circuit for synthesizing multiple beams; a calibration signal coupling part, provided between said multi-beam synthesizing circuit and said antenna elements, for inputting a calibration signal; a calibration signal generator; a calibration amount calculator; wherein said calibration signal generator applies a calibration signal output to a plurality of said calibration signal coupling parts successively, said calibration amount calculator calculating a calibration amount for each of receiving systems from baseband signals of said receiving systems connected to the outputs of said multi-beam synthesizing circuit every time said calibration signal output is applied to said calibration signal coupling part, and calibration to said receiving systems being performed by using a mean value of calculated calibration amounts.

[0022] According to the invention as claimed in claim 2, calibration amount calculation of the receiving system is performed a plurality of times and the mean value is used as the calibration amount of the receiving system. Therefore, more reliable calibration can be realized.

[0023] The invention as claimed in claim 3 is the adaptive array antenna as claimed in one of claim 1 and 2, wherein an FFT processing circuit is provided for performing calculation of multi-beam resolution within a base station in the outside of said receiving systems of said array antenna.

[0024] According to the invention as claimed in claim 3, since the FFT processing circuit is provided for performing multi-beam resolution calculations within the base station, calibration and adaptive signal processing can be performed for each antenna element.

[0025] The invention as claimed in claim 4 is a calibration amount calculation method in a receiving system of an array antenna having a plurality of antenna elements, said calibration amount calculation method characterized by: applying a calibration signal generated by a calibration signal generator to a calibration signal coupling part provided in one antenna element; sending said calibration signal to a plurality of said receiving systems by a multi-beam synthesizing circuit; and calculating a calibration amount of each of said receiving systems from baseband signals obtained by detecting calibration signals of said receiving systems.

[0026] According to the invention as claimed in claim 4, individual variation between calibration signals are eliminated and reliable calibration can be performed.

[0027] The invention as claimed in claim 5 is a calibration amount calculation method in a receiving system of an array antenna having a plurality of antenna elements, comprising: applying a calibration signal to calibration signal coupling parts provided in a plurality of antenna elements successively; sending said calibration signal to a plurality of said receiving systems by a multi-beam synthesizing circuit provided in an array antenna simultaneously; calculating, by a calibration amount calculator connected to a plurality of said receiving systems, calibration amounts of said receiving systems from baseband signals obtained by detecting cal-

ibration signals of said receiving systems; using a mean value of said calibration amounts as a calibration amount of said receiving system.

[0028] According to the invention as claimed in claim 5, calibration amount calculation of the receiving system is performed a plurality of times and the mean value is used as the calibration amount of the receiving system. Therefore, more reliable calibration can be realized.

[0029] The invention as claimed in claim 6 is the calibration amount calculation method of said receiving systems of said adaptive array antenna as claimed in claim 4 or 5, wherein verification of calibration amount calculation is available by providing, in the outside of said receiving systems of said array antenna, an FFT processing circuit for performing calculation of multi-beam resolution within a base station.

[0030] According to the invention as claimed in claim 6, since the FFT processing circuit is provided for performing multi-beam resolution calculations within the base station, calibration and adaptive signal processing can be performed for each antenna element. In addition, calibration amount calculation can be verified.

[0031] The invention as claimed in claim 7 is a calibration method for performing calibration of a receiving system of an array antenna by performing adaptive signal processing, said calibration method characterized by performing adaptive signal processing after subtracting said calibration amount calculated by the method claimed in claim 4 or 5 as an adaptive signal processing amount when performing adaptive signal processing for an adaptive array antenna.

[0032] According to the invention as claimed in claim 7, calibration can be performed within adaptive signal processing without using waits for calibration.

BRIEF DESCRIPTION OF THE DRAWINGS

[0033] Other objects, features and advantages of the present invention will be apparent by reading the following description in conjunction with the accompanying drawings.

[0034] Fig.1 is a configuration example (a first example) of an adaptive array antenna which has wide element spacing and narrow element spacing according to the present invention, and performs adaptive signal processing.

[0035] Fig.2 is a configuration example (a second example) of an adaptive array antenna which has wide element spacing and narrow element spacing, and performs adaptive signal processing.

[0036] Fig.3 is a configuration example (a third example) of an adaptive array antenna which has wide element spacing and narrow element spacing, and performs adaptive signal processing.

[0037] Fig.4 is a configuration example (a first example) of an adaptive array antenna which performs calibration processing of the present invention.

[0038] Fig.5 is a configuration example (a second ex-

ample) of an adaptive array antenna which performs calibration processing of the present invention.

[0039] Fig.6 is a configuration example (a third example) of an adaptive array antenna which performs calibration processing of the present invention.

[0040] Fig.7 is a configuration example (a fourth example) of an adaptive array antenna which performs calibration processing of the present invention.

[0041] Fig.8 is a configuration example of an adaptive array antenna which achieves the object of the present invention.

[0042] Fig.9 is a flowchart for explaining a method (a first method) of calibration amount calculation.

[0043] Fig.10 is a flowchart for explaining a method (a second method) of calibration amount calculation.

[0044] Fig.11 is a flowchart for explaining a method (a third method) of calibration amount calculation.

[0045] Fig.12 is a configuration example of a conventional adaptive array antenna (a first example) of narrow element spacing.

[0046] Fig.13 is a configuration example of a conventional adaptive array antenna of wide element spacing.

[0047] Fig.14 is a configuration example of a conventional maximum ratio synthesizing type adaptive array antenna of wide element spacing.

[0048] Fig.15 is a configuration example of a conventional adaptive array antenna (a second example) of narrow element spacing.

[0049] Fig.16 is a configuration example of a conventional interference suppression type adaptive array antenna of wide element spacing.

[0050] Fig.17 is a diagram for explaining a conventional calibration method.

[0051] Fig.18 is a diagram for explaining a calibration signal coupling part.

[0052] Fig.19 is a diagram for explaining an example of a multi-beam synthesizing circuit (butler matrix).

PREFERRED EMBODIMENTS FOR CARRYING OUT THE INVENTION

[0053] In the following, embodiments of the invention of the parent application EP-A-1014485 will be described with reference to figures. (first embodiment)

[0054] Fig.1 shows the first embodiment which is an eight element array antenna. An array antenna #1 comprises antenna elements 51-54 and an array antenna #2 comprises antenna elements 55-58. The spacing between the array antenna elements of the array antenna #1 and the array antenna #2 is about $\lambda/2$. The array antenna #1 is placed at a distance (of several λ s) from the array antenna #2 such that the correlation becomes small enough to be negligible.

[0055] Signals from each of the antenna elements 51-58 are synthesized by the signal adder 59 via the waits 61-68 which adjust phase and amplitude of antenna output and output. The wait of the waits 61-68 is controlled by the adaptive signal processing device 60. The

adaptive signal processing may be the interference suppression, tracking type or the maximum gain tracking type.

[0056] In this example, all outputs from the eight elements are converted into baseband simultaneously and adaptive processing is performed. Calibration relating to the second object of the present invention is necessary in each array antenna. However, it is not necessary between the array antennas. In a multipath environment, each array antenna can augment gain and can form the main beam.

[0057] Concerning the array antennas, in this example, consider that uncorrelated four element array antenna is added. Therefore, the same interference characteristics as shown in Fig.18 can be obtained. That is, the array antenna has the capability of removing interference waves from the same direction. In addition, since the array antenna is uncorrelated, it has diversity effect pertaining to fading. In the algorithm of the array antenna, diversity, main beam tracking, removal of interference waves can be performed together without concerning for the difference.

(second embodiment)

[0058] Fig.2 shows the second embodiment. The number of elements is eight which is the same as the first embodiment. The arrangement of the antenna is the same, but the signal synthesizing method is different.

[0059] Each of an array antenna #1 and an array antenna #2 operates according to an independent algorithm. That is, outputs from antenna elements 51-54 of the array antenna #1 are synthesized at a signal adder 61 via waits 81-84. The waits 81-84 are controlled by an adaptive signal processing device 83. Outputs from antenna elements 55-58 of the array antenna #2 are synthesized at a signal adder 62 via waits 85-88. The waits 85-88 are controlled by an adaptive signal processing device 84. The adaptive signal processing device 84 operates in isolation from the adaptive signal processing device 83. At this stage, since the correlation between antenna elements of each array antenna is high, fading can not be compensated for and the interference waves from the same direction can not be removed.

[0060] Baseband outputs of the signal adder 61 and the signal adder 62 are synthesized by the signal adder 71 via waits 90, 91. The waits 90, 91 are controlled by an adaptive signal processing device 70. Since the envelopes of input signals of the adaptive array antennas are uncorrelated, the baseband outputs of the signal adder 61 and the signal adder 62 are uncorrelated. Therefore, fading can be compensated for at this stage. In addition, each adaptive array antenna can remove interference waves from the same direction at this stage.

(third embodiment)

[0061] Fig.3 shows the third embodiment. The config-

uration is the same as that of the second embodiment. However, each of the four element adaptive array antennas does not operate independently. That is, the same adaptive signal processing device 88 controls waits 81-84 of antenna elements 51-54 of an array antenna #1 and waits 85-88 of antenna elements 55-58 of an array antenna #2. A two element algorithm of the after stage selects adaptively an adaptive array antenna to be operated by determining magnitude of the power of the array antennas. By referring to waits of one side, calculation amount is decreased.

[0062] In the above-mentioned embodiment, the spacing of the antenna elements is $\lambda/2$, which is a distance for exhibiting very high correlation. However, the distance is not necessarily exactly $\lambda/2$. The distance may be around $\lambda/2$ as long as the effect of the present invention can be obtained. The spacing between the array antennas is large enough for making the correlation low enough. "The correlation low enough" does not mean no correlation. The correlation may be substantively small enough as long as the effect of the present invention can be obtained.

[0063] In addition, the present invention is not limited to the above-mentioned embodiment, that is, the configuration of eight antenna elements and two array antennas.

[0064] In the following, embodiments of the present invention will be described with reference to figures.

(fourth embodiment)

[0065] The fourth embodiment takes a configuration wherein an after-mentioned multi-beam synthesizing circuit is provided after the array antenna, signals are transmitted to an indoor part of the base station via cables, and the signals are extracted as element outputs after performing after-mentioned FFT by baseband. A calibration signal is input from a calibration signal coupling part which is located between the array antenna and the multi-beam synthesizing circuit.

[0066] The characteristics of this method are that a signal input to an element antenna is transmitted to the indoor part of the base station after being distributed to all cables via the multi beam synthesizing circuit. When a signal is input in the multi-beam synthesizing circuit, signals which have a constant phase difference are output at a plurality of output terminals. That is, it becomes possible to calibrate receiving systems for actual signals by one signal. Here, the receiving system is a series of receiving circuits connected to the output of the multi-beam synthesizing circuit. That is, the receiving system is a system including a filter, a high frequency amplifier, a mixer, a filter, an intermediate frequency amplifier and an AD converter.

[0067] Fig.4 shows the fourth embodiment. The number of elements of the array antenna is four (#1-#4). A signal from a calibration signal generator 101 is applied to the multi-beam synthesizing circuit 162 via a cal-

ibration signal input terminal 150. The multi-beam synthesizing circuit 152 is a four element butler matrix as shown in Fig. 19. The butler matrix is configured by hybrids 181-184. Since it is well known, a description of the operation will not be provided. The outputs from the multi-beam synthesizing circuit 152 are applied to filters 103-106, high frequency amplifier 107-110 and a distribution and synthesizing part 134. The signals distributed here are AD-converted via mixers 111-114, filters 115-118 and intermediate frequency amplifier 119-122. In addition, FFT (Fast Fourier Transform) is performed on the signals after waits are added by waits 128-131 such that the signals are converted to normal signals of an adaptive array antenna. FFT (Fast Fourier Transform) 153 performs conversion which is reverse to that of the multi-beam synthesizing circuit. That is, the signal of the calibration signal input terminal 150 is converted by the multi-beam synthesizing circuit 152 and is output to the filters 103-106 with a constant phase. The FFT here performs reverse conversion of that. As shown Fig. 4, since the calibration signal is applied only to the receiving system #4, a signal appears only on the receiving system #4 if calibration is properly performed.

[0068] In the same way as shown in Fig. 17, a calibration amount calculator 154 calculates the calibration amount. An adaptive signal processing device 155 stores the calibration amount in a calibration table (not shown in the figure) and controls waits 128-131 by subtracting the calibration amount when performing adaptive signal processing.

[0069] The calibration may be performed by providing a wait for the calibration other than the waits for adaptive signal processing and controlling phase and amplitude of the wait for the calibration.

[0070] According to the fourth embodiment, the signal from the calibration signal generator is input to the calibration signal input terminal 150 between the antenna element #4 and the multi-beam synthesizing circuit 152, output from the four different output terminals by the multi-beam synthesizing circuit 152 with different phases and transmitted to each receiving system.

[0071] Therefore, since the individual variation between the calibration signals does not exist, highly reliable calibration can be performed by monitoring whether the phase relation is kept at a baseband part.

(fifth embodiment)

[0072] In the fourth embodiment, if the calibration signal is applied to the remaining antenna elements, signals having another phase relation appear at a plurality of terminals. In the fifth embodiment, by applying the calibration signal to a plurality of antennas in such a way, a plurality of calibration values can be obtained. Then, reliable calibration can be performed by averaging the result. Since the multi-beam outputs are synthesized just after the array antenna in the same way as the fourth embodiment, signals are transmitted to each receiving

system while keeping the phase amplitude relation between antenna elements. That is, the pattern of each beam is preserved without being disturbed. Only phase ratio and phase difference between beams are disturbed. Only the value between the beams needs to be calibrated.

[0073] Fig. 5 shows the fifth embodiment. Fig. 5 shows a configuration which is almost the same as that of the fourth embodiment. The difference is that calibration signals are input via four routes in the fifth embodiment. That is, antenna elements have calibration signal input terminals 186-189. The output from the calibration signal generator 101 is applied successively to the terminals 186-189 by using a switching circuit 181. That is, the output from the calibration signal generator 101 is applied to the calibration signal input terminals 186-189 successively. At this time, function of the calibration signal applied to each calibration signal coupling part is the same as that of the calibration signal in Fig. 4. A calibration amount calculator 170 calculates the calibration amounts based on the calibration signal applied successively and calculates a mean value of the calibration amounts after a cycle. The mean value is used as the calibration amount for use.

[0074] In the fifth embodiment, each of the calibration signals of the four routes is applied to a calibration signal input terminal of four calibration signal input terminals with different phase relation. By calibrating by switching the four routes, reliability is improved since the average of the calibration amounts is available. In this case, since the calibration signals of the four routes are not used simultaneously, calibration accuracy is not affected even when the calibration cables have individual variations.

(sixth embodiment)

[0075] In the case wherein the multi-beam output is used as it is, the FFT circuit of the after stage is not necessary and the configuration becomes simpler.

[0076] Fig. 6 shows the sixth embodiment. The embodiment is an example of a configuration of an adaptive array antenna of a beam space type using a multi-beam synthesizing circuit. As compared with the fourth embodiment, the sixth embodiment does not have the FFT circuit.

(seventh embodiment)

[0077] Fig. 7 shows the seventh embodiment. Similar to the sixth embodiment, the seventh embodiment is an other example of a configuration of an adaptive array antenna of a beam space type using a multi-beam synthesizing circuit. As compared with the fifth embodiment, the seventh embodiment does not have the FFT circuit.

[0078] In the following, flowcharts of representative calibration amount calculation methods will be de-

scribed.

[0079] Fig.9 is a flowchart of the calibration amount calculation method in the case wherein the calibration signal is applied to one antenna element.

[0080] The calibration signal generated by the calibration signal generator is applied to the calibration signal coupling part which is provided in the antenna element (S10). The calibration signal is sent to a plurality of receiving systems simultaneously by the multi-beam synthesizing circuit (S11). Then, the calibration signal is detected in each of the plurality of receiving systems (S12). Finally, the calibration amounts of the receiving systems are calculated (S13).

[0081] Fig.10 is a flowchart of the calibration amount calculation method in the case wherein the calibration signal is applied to a plurality of antenna elements.

[0082] The calibration signal is applied to the calibration signal coupling parts provided in a plurality of antenna elements successively and it is determined whether the calibration signal is applied to every antenna element (S20). If NO, the calibration signal is sent to a plurality of receiving systems simultaneously by the multi-beam synthesizing circuit (S21). Then, the calibration signal is detected in each of the plurality of receiving systems and the calibration amounts of each receiving system are calculated (S22). The process is repeated until the calibration signal is applied to every antenna element. When the calibration signal is applied to every antenna element (YES in S20), the mean value of the calibration amounts is regarded as the calibration amount (S23).

[0083] Fig.11 is a flowchart of the calibration amount calculation method in the case wherein the FFT processing circuit is provided outside of the receiving system of the array antenna for performing multi-beam resolution calculation in the base station.

[0084] For example, as shown in Fig.9, the calibration amount is calculated for each antenna element (S30). At the time, a signal of a receiving system of the array antenna which is not calibrated is checked such that the calibration amount calculation is verified (S31).

[0085] As mentioned above, according to the embodiments of the present invention, it becomes possible to achieve gain of the array antenna, track beam, have diversity effects and suppress the interference waves from the same direction.

[0086] In addition, the amount of signal processing can be decreased. As a result, the application field of the array antenna can be extended.

[0087] Further, according to the above-mentioned embodiments, it is possible to calibrate a plurality of systems of a current transmission system by using only one calibration signal route. By using calibration signals of a plurality of routes, more reliable calibration result can be obtained since the calibration data can be averaged. When multi-beam output is used as it is herein, the FFT circuit in the after stage is not necessary and the configuration becomes simpler.

[0088] Next, a configuration of an array antenna which can achieve the object of the present invention is shown in Fig. 8.

[0089] The configuration includes array antennas #1, #2, multi-beam circuits 201, 202, #1-#4 of receiving systems 203, #1-#4 of receiving systems 204, calibration signal generators 205, 206, calibration amount calculator 207, 208, an adaptive signal processing device 209, calibration signal coupling parts 210, 211, waits 212 and a signal adder 213. The configuration is not limited to that shown in Fig.8. Combinations from Fig.1-Fig.3 and Fig.4-Fig.7 can be used.

[0090] The array antennas #1, #2 are array antennas each of which array antenna has a plurality of antenna elements spaced at intervals at which the correlation is high. The spacing between the array antennas #1, #2 has a distance such that correlation can be negligible.

[0091] The operation can be considered as the combination of the operations of Fig.1-Fig.3 and Fig.4-Fig.7. Therefore, the description of the operation will not be given.

[0092] The adaptive signal processing device 209 may perform adaptive signal processing by using an adaptive signal processing amount obtained by subtracting the calibration amount calculated by the calibration amount calculators 207, 208.

[0093] The present invention is not limited to the specifically disclosed embodiments, and variations and modifications may be made without departing from the scope of the invention.

Claims

1. An adaptive array antenna characterized in that said adaptive array antenna comprises:

an array antenna having a plurality of antenna elements;
a multi-beam synthesizing circuit for synthesizing multiple beams;
a calibration signal coupling part, provided between said multi-beam synthesizing circuit and said antenna element, for inputting a calibration signal;
a calibration signal generator;
a calibration amount calculator;

wherein said calibration signal generator is arranged to apply a calibration signal output to said calibration signal coupling part,

said calibration amount calculator being arranged to calculate a calibration amount for each of receiving systems from baseband signals of said receiving systems connected to the outputs of said multi-beam synthesizing circuit and to perform calibration to said receiving systems.

2. An adaptive array antenna as claimed in Claim 1,
wherein said calibration signal generator is ar-
ranged to apply a calibration signal output to a plu-
rality of said calibration signal coupling parts suc-
cessively,
said calibration amount calculator being ar-
ranged to calculate a calibration amount for each of
the receiving systems from baseband signals of
said receiving systems connected to the outputs of
said multi-beam synthesizing circuit every time said
calibration signal output is applied to said calibra-
tion signal coupling part, and calibration to said re-
ceiving systems being performed by using a mean
value of calculated calibration amounts. 5
3. An adaptive array antenna as claimed in one of
claims 1 and 2, wherein an FFT processing circuit
is provided for performing calculation of multi-beam
resolution within a base station in the outside of said
receiving systems of said array antenna. 10
4. A calibration amount calculation method in a receiv-
ing system of an array antenna having a plurality of
antenna elements, said calibration amount calcula-
tion method characterized by: 15

applying a calibration signal generated by a cal-
ibration signal generator to a calibration signal
coupling part provided in one antenna element;
sending said calibration signal to a plurality of
said receiving systems by a multi-beam synthe-
sizing circuit; and 20
calculating a calibration amount of each of said
receiving systems from baseband signals ob-
tained by detecting calibration signals of said
receiving systems. 25
5. A calibration amount calculation method as claimed
in Claim 4, the multi-beam synthesizing circuit being
provided in an array antenna; 30
comprising applying a calibration signal to cal-
ibration signal coupling parts provided in a plurality
of antenna elements successively;
calculating the calibration amounts by a cal-
ibration amount calculator connected to a plurality
of said receiving systems; 35
and using a mean value of said calibration
amounts as a calibration amount of said receiving
system. 40
6. The calibration amount calculation method as
claimed in claim 4 or 5, wherein verification of cali-
bration amount calculation is available by providing,
in the outside of said receiving systems of said array
antenna, an FFT processing circuit for performing
calculation of multi-beam resolution within a base
station. 45
7. A calibration method for performing calibration of a
receiving system of an array antenna by performing
adaptive signal processing, said calibration method
characterized by performing adaptive signal
processing after subtracting said calibration
amount calculated by the method claimed in claim
4 or 5 as an adaptive signal processing amount
when performing adaptive signal processing for an
adaptive array antenna. 50

FIG. 1

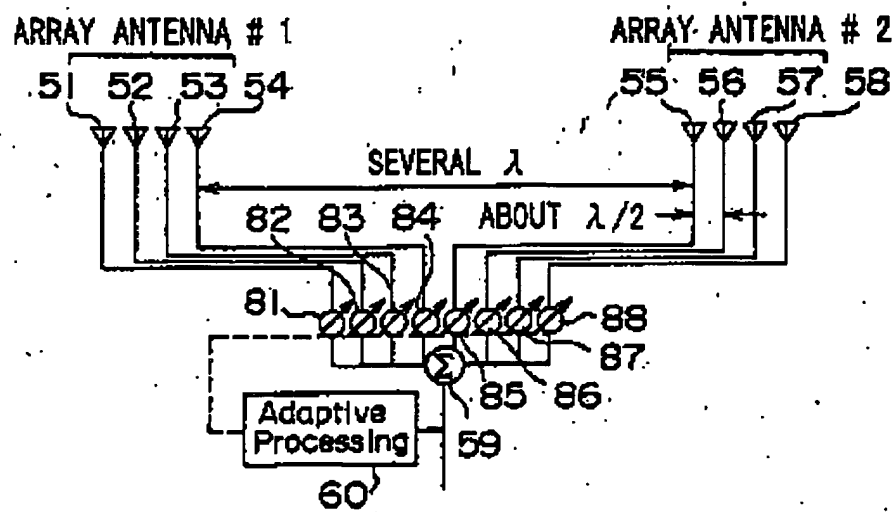


FIG. 2

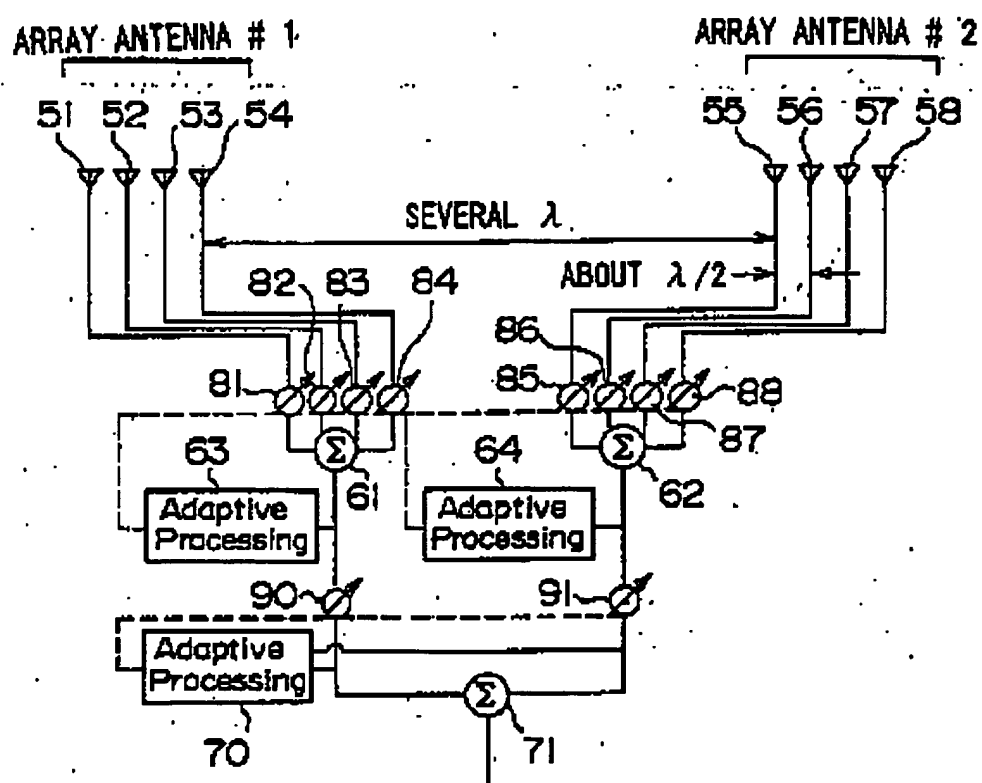


FIG. 3

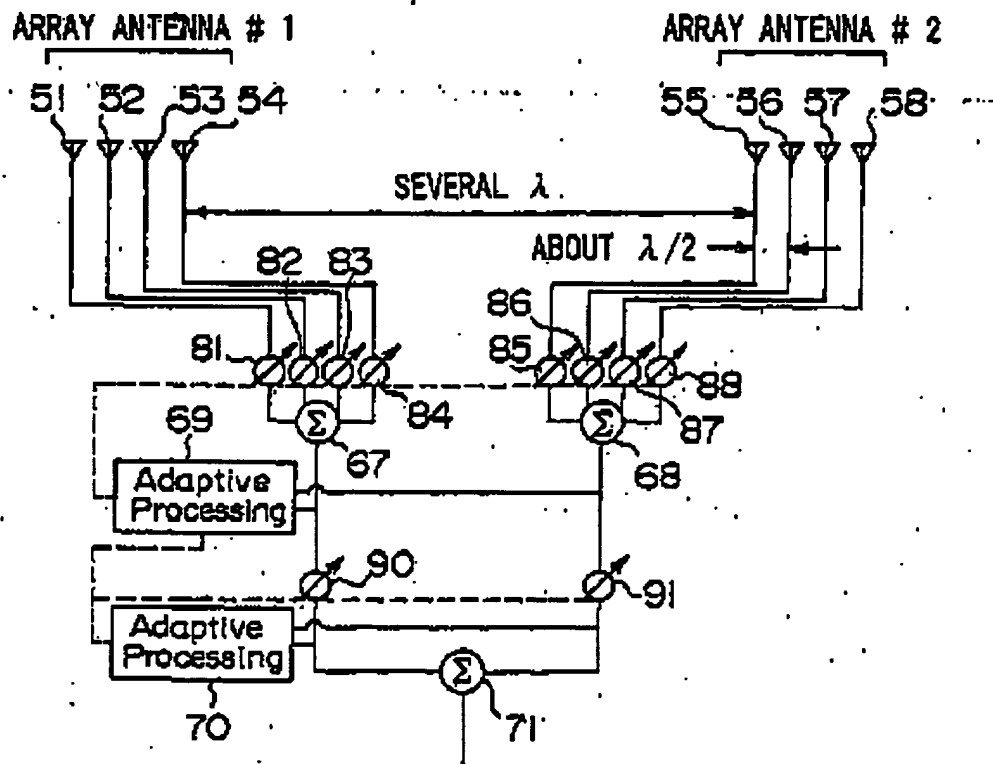


FIG.4

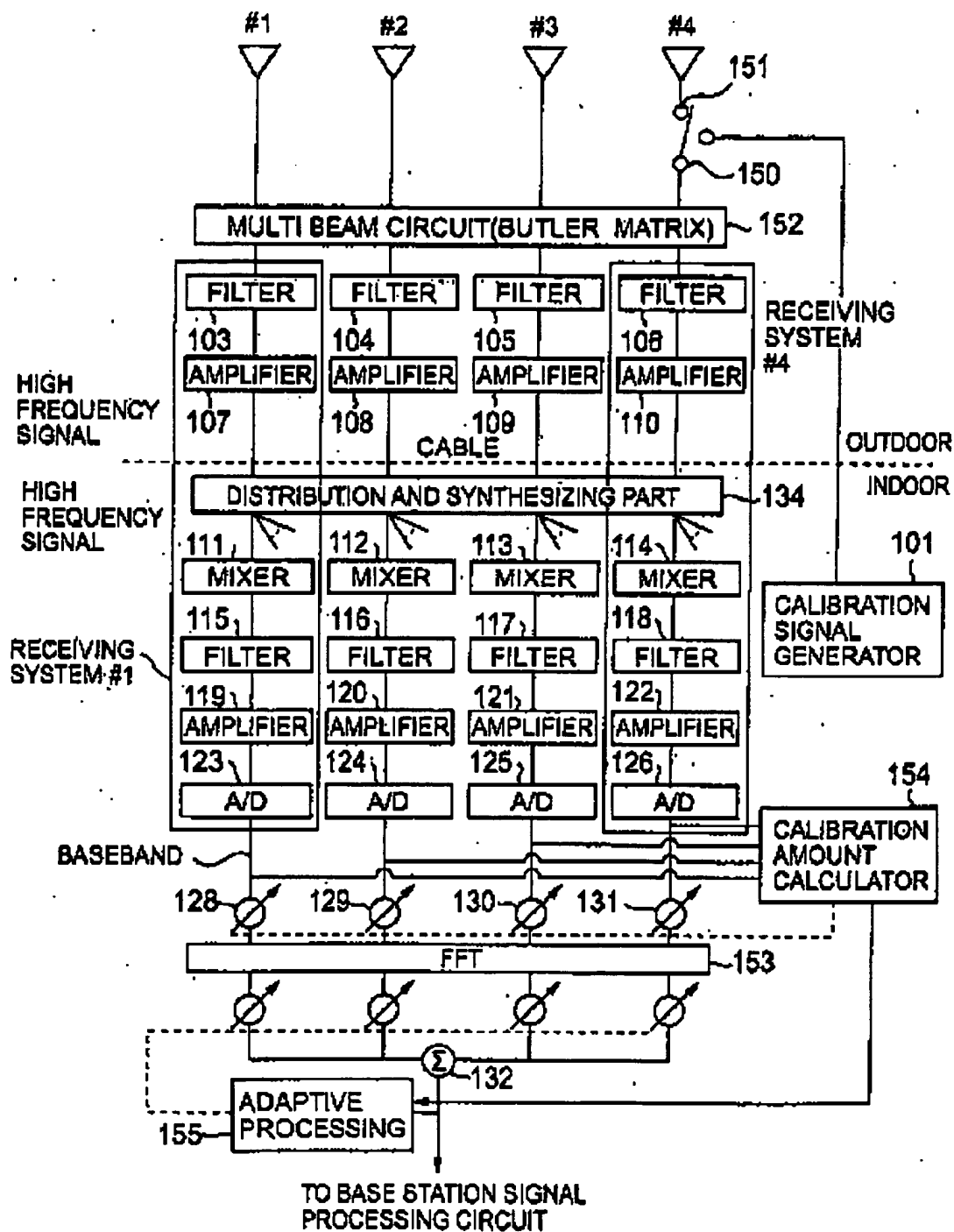


FIG.5

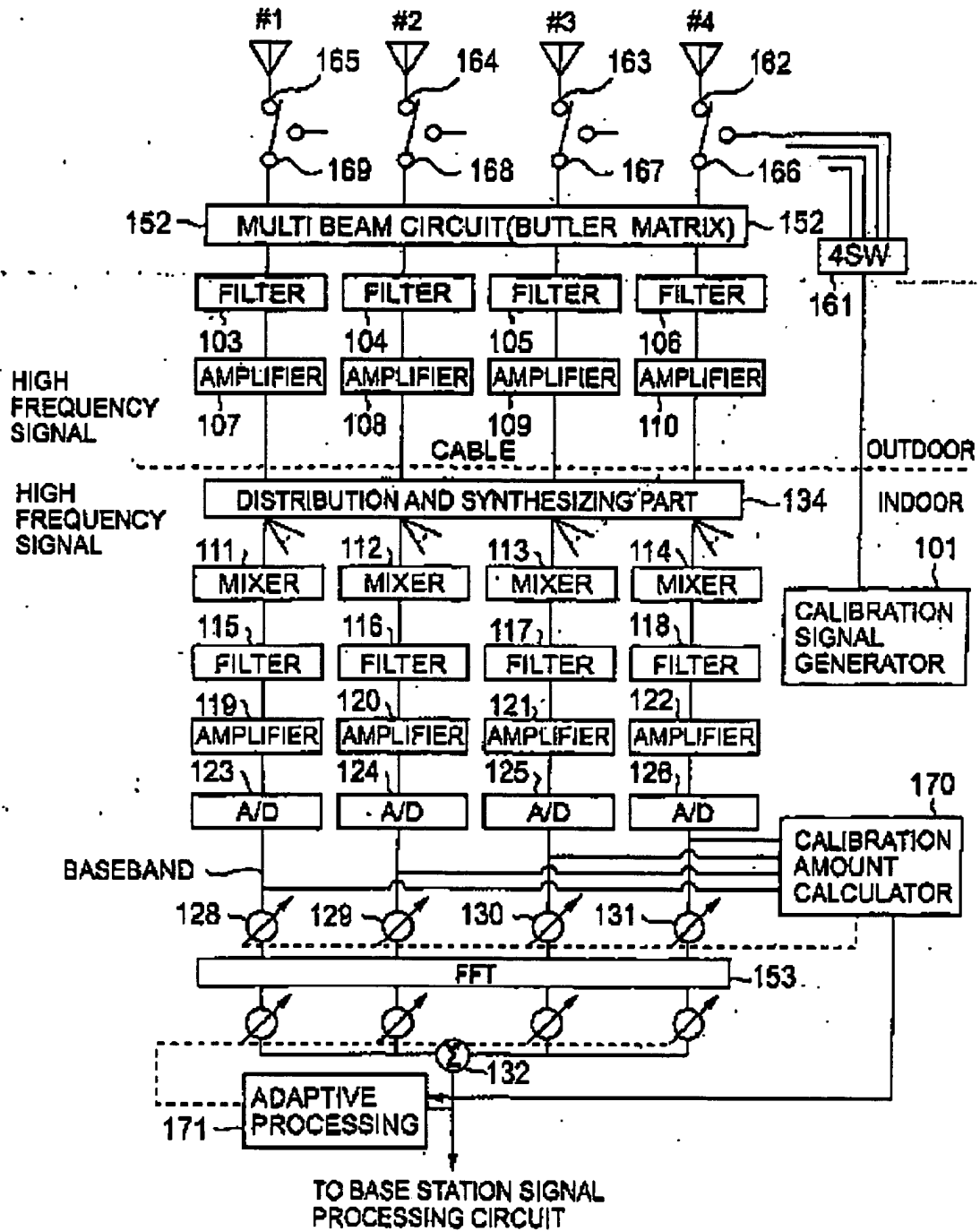


FIG.6

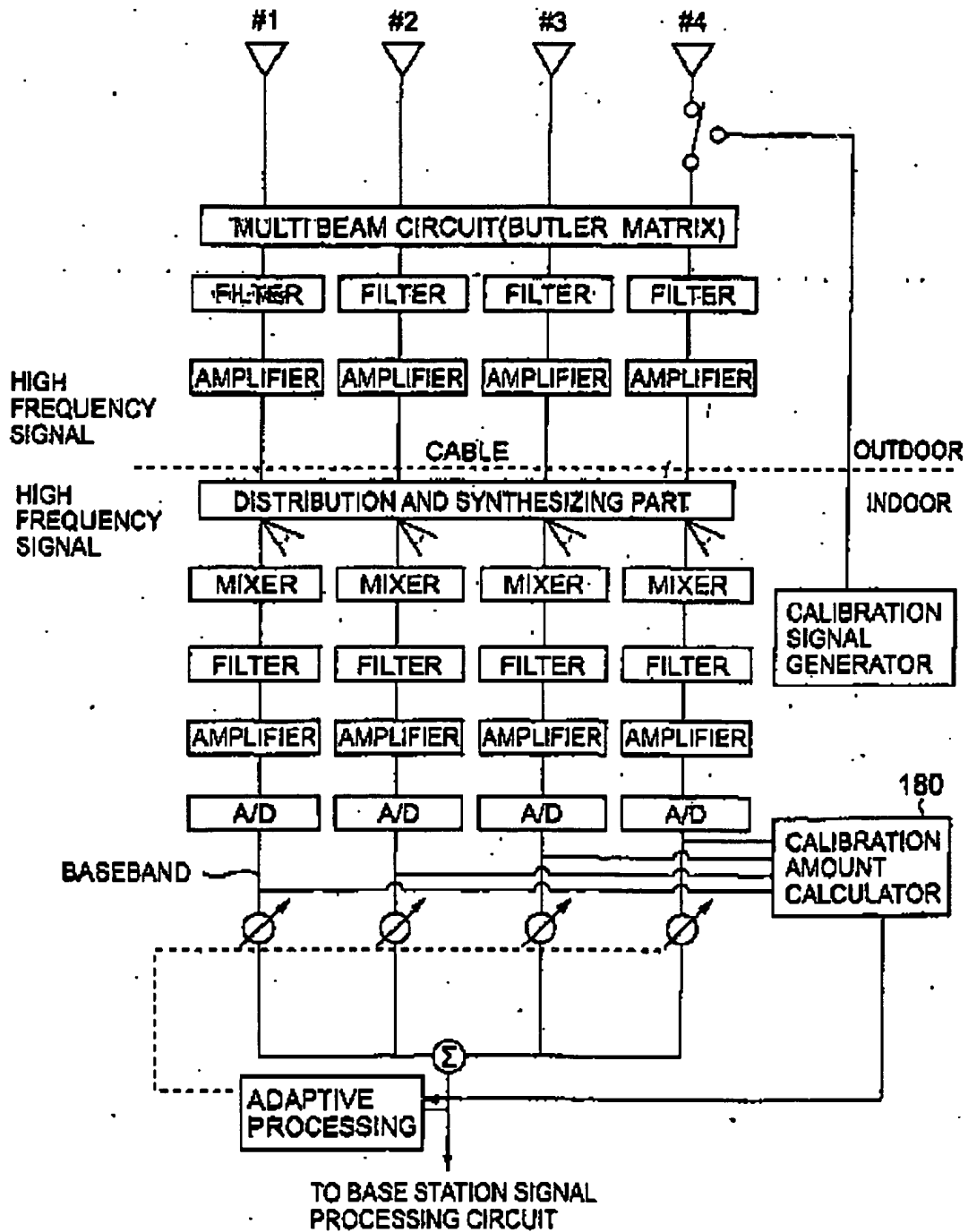


FIG.7

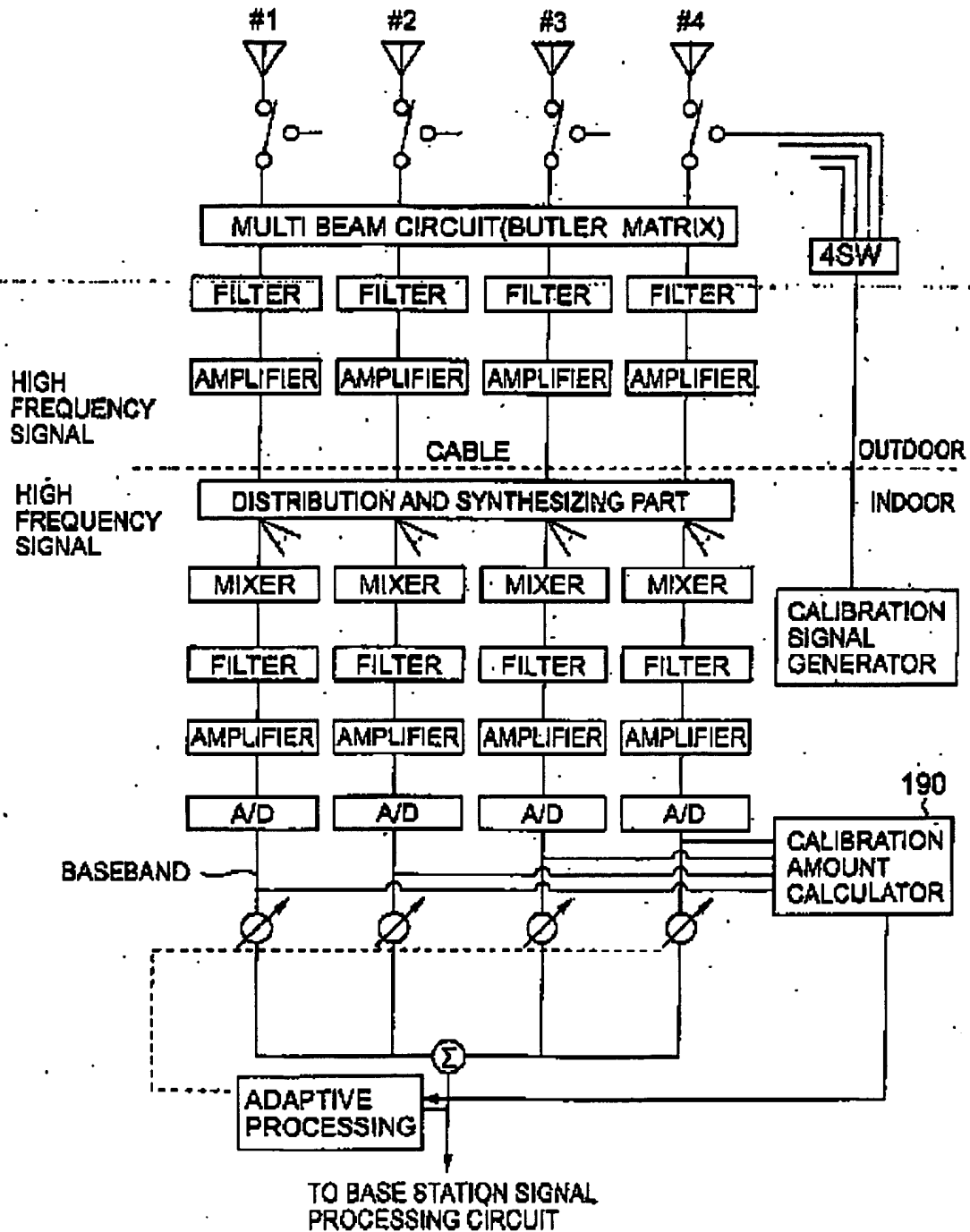


FIG. 8

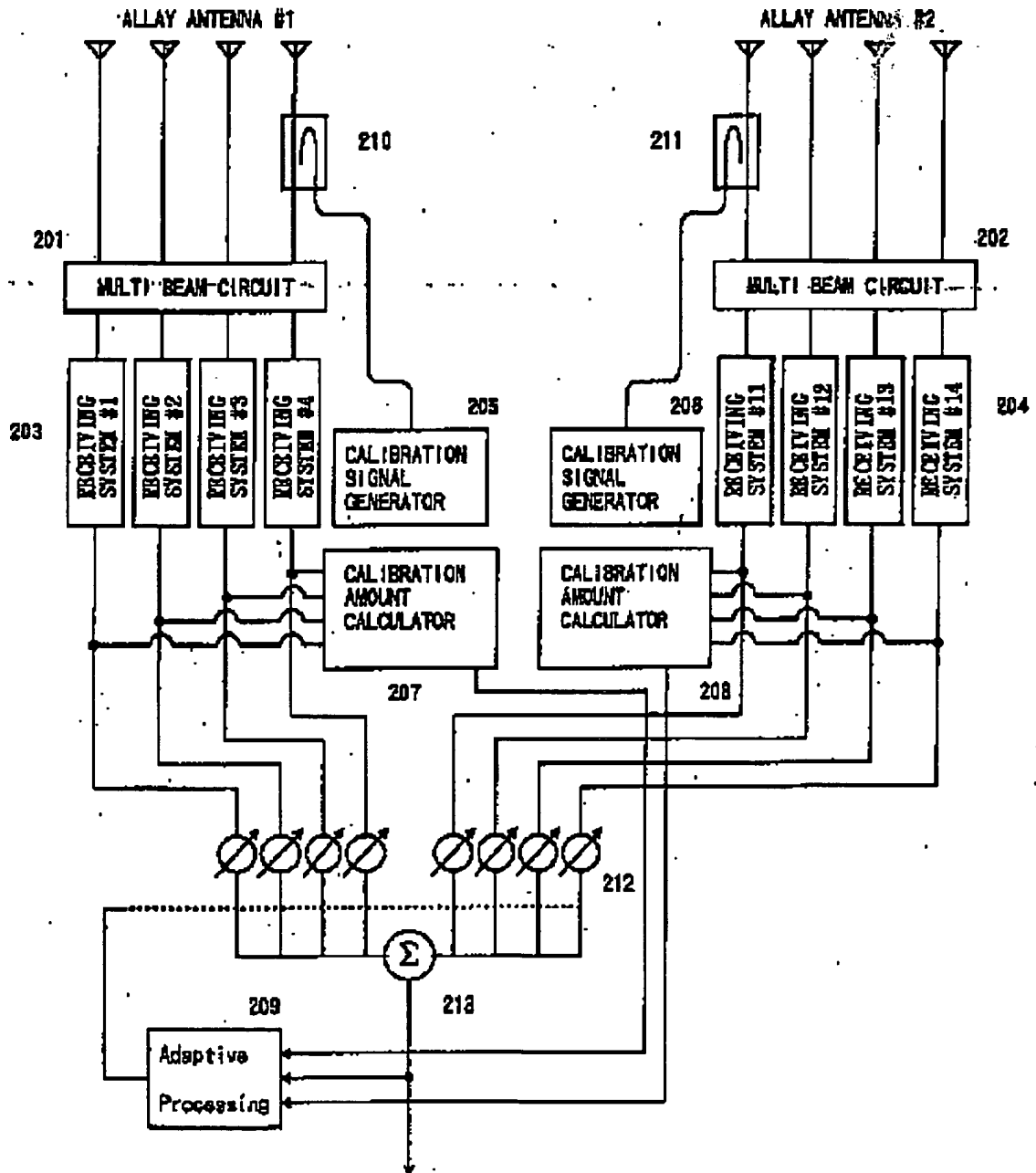


FIG. 9

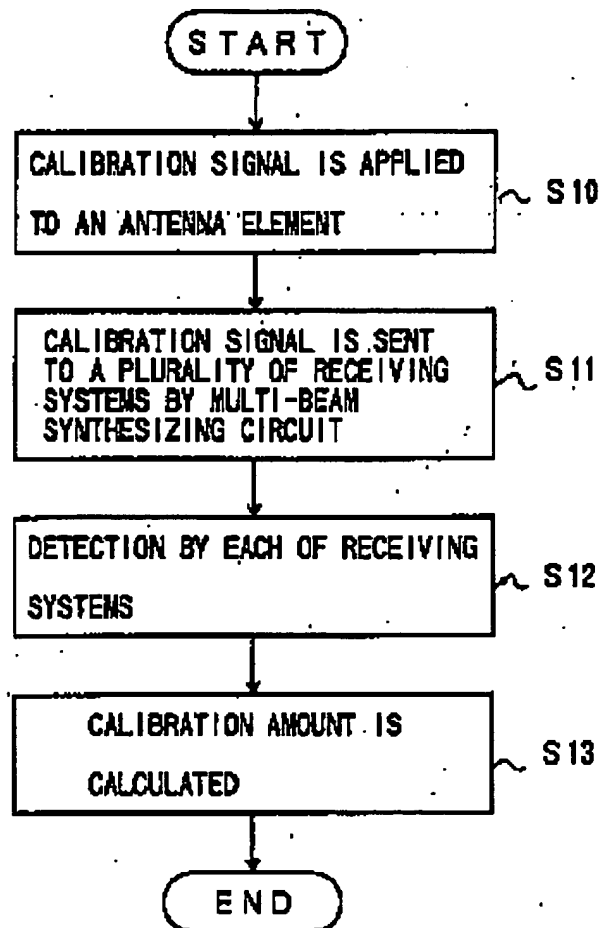


FIG. 10

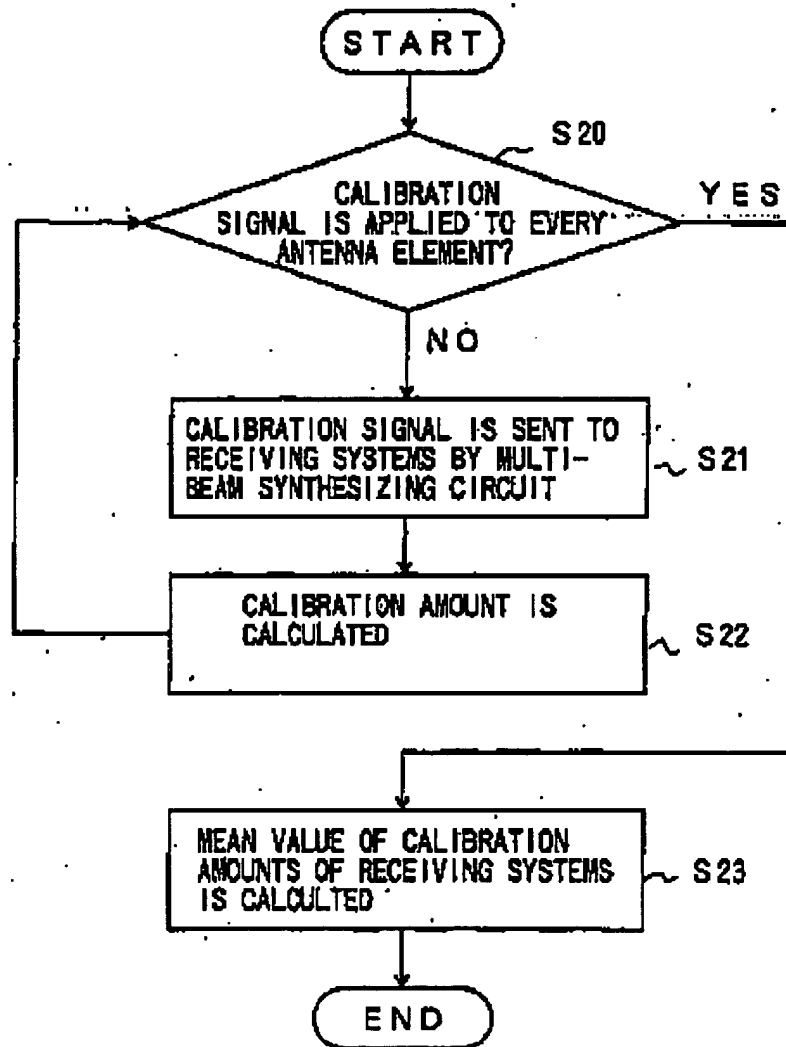


FIG. 11

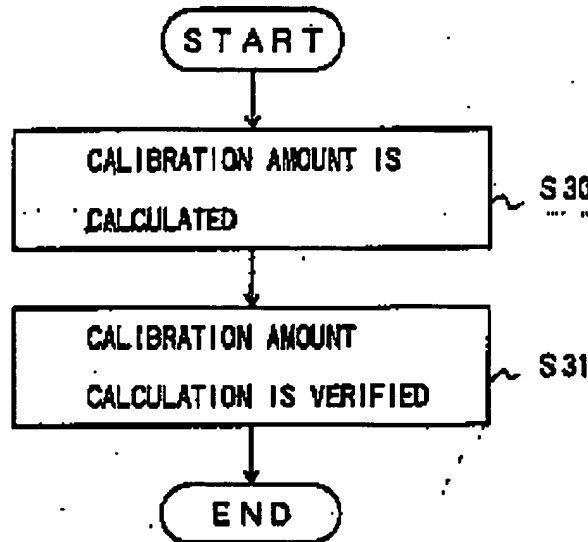


FIG. 12

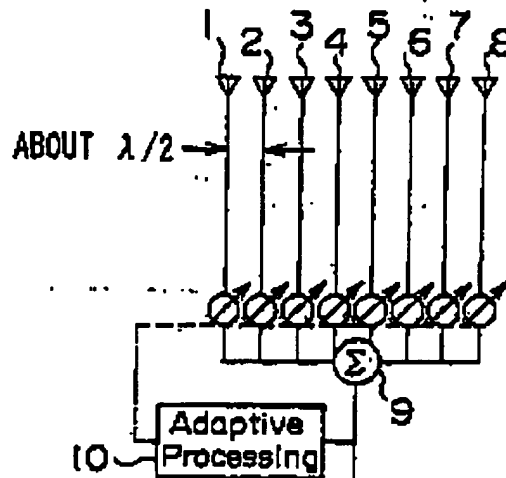


FIG. 13

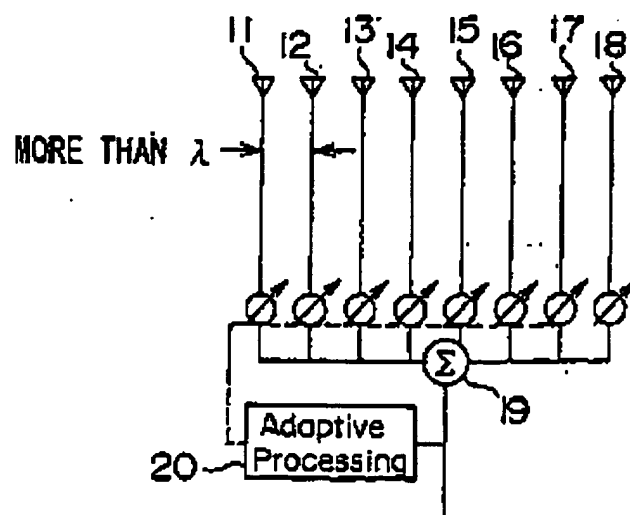


FIG. 14

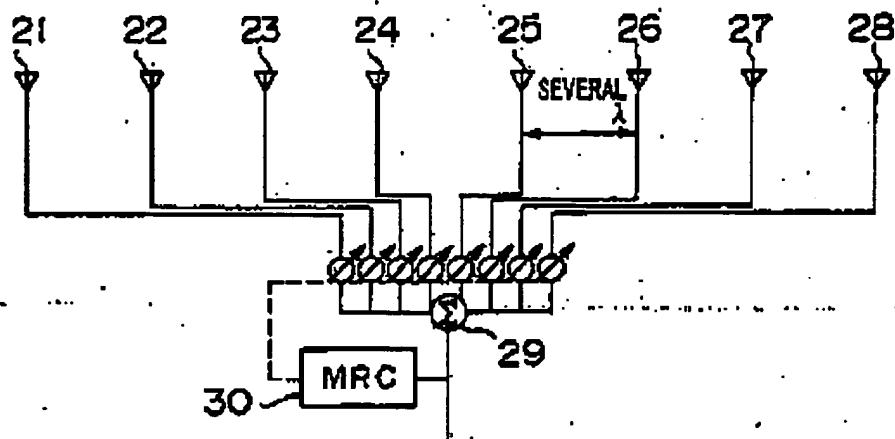


FIG. 15

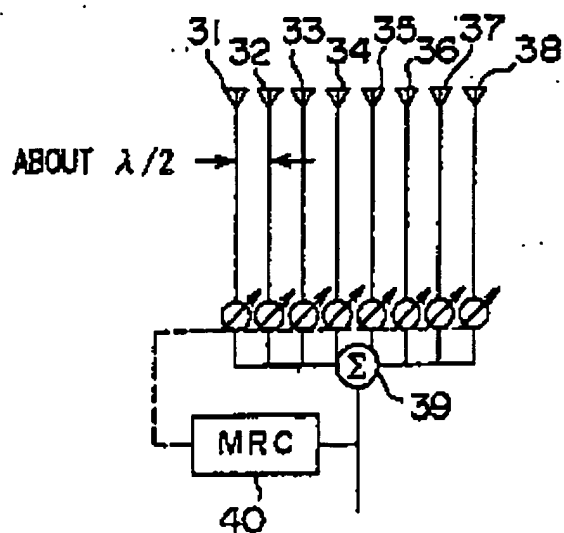


FIG. 16

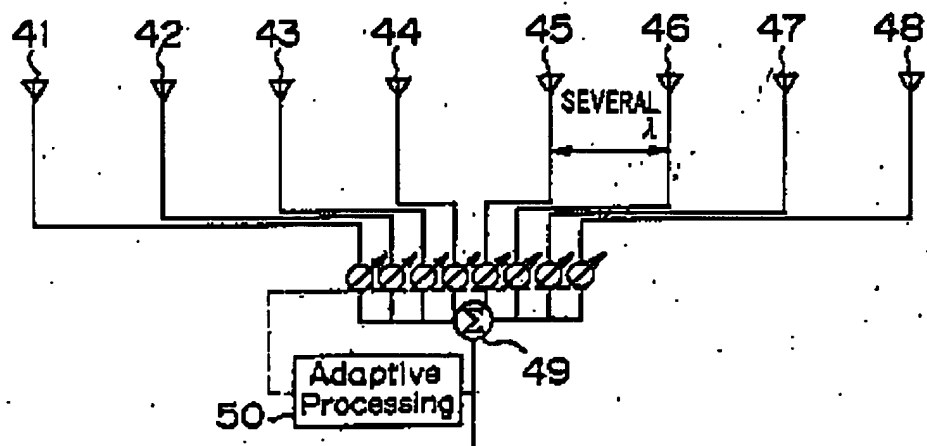


FIG.17

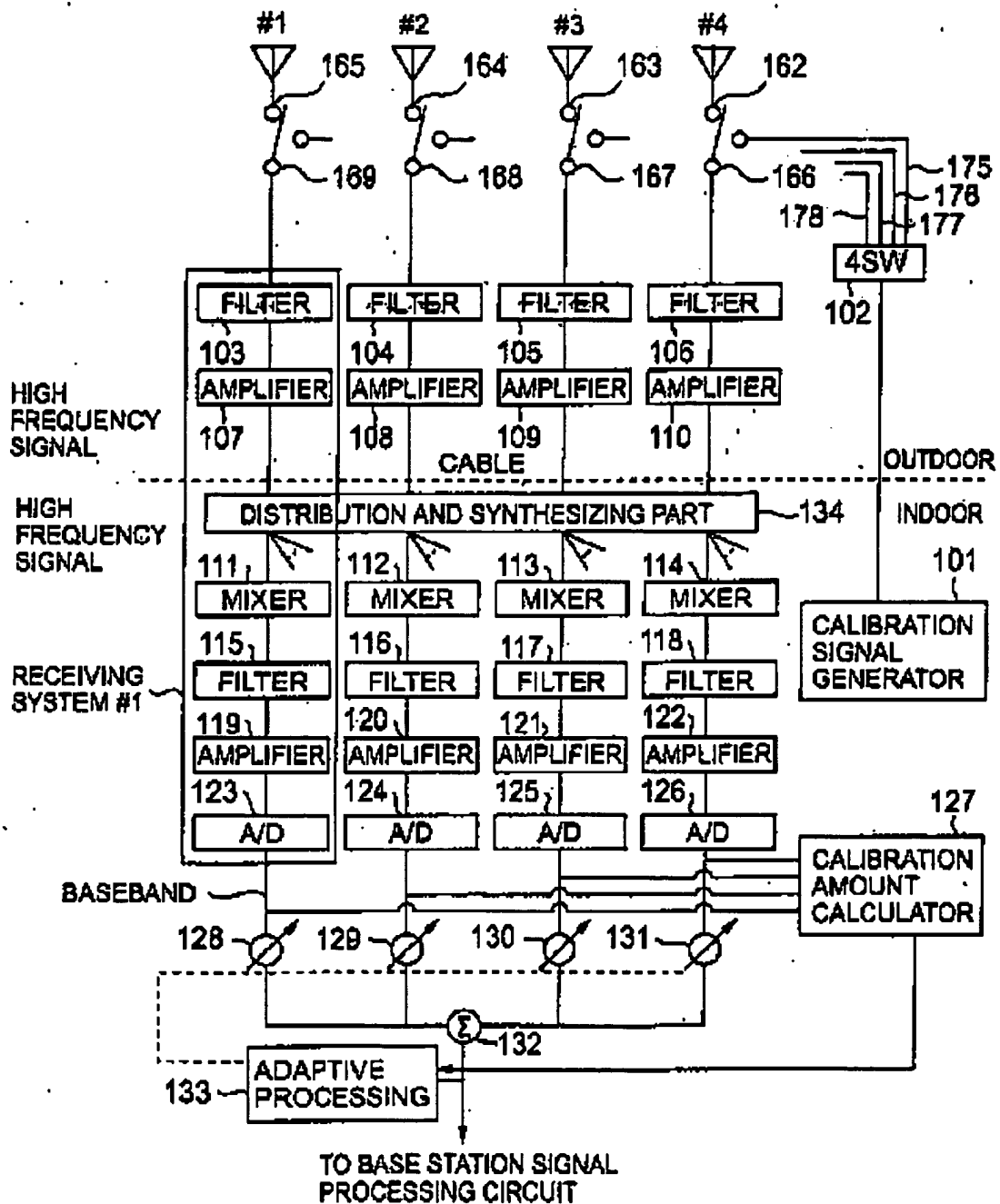


FIG. 18A

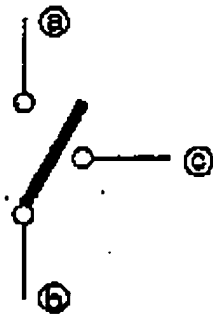


FIG. 18B

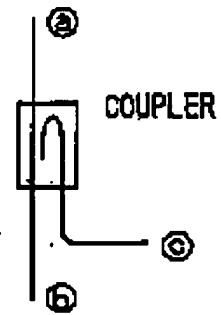
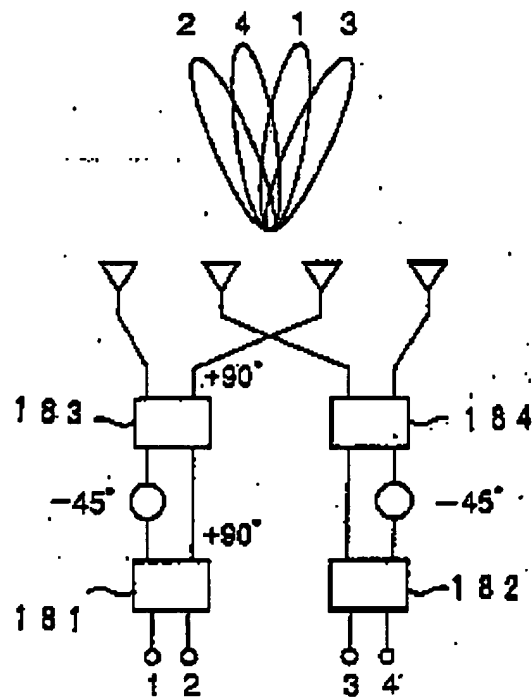


FIG. 19





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 03 01 9890

| DOCUMENTS CONSIDERED TO BE RELEVANT | | | |
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| Category | Citation of document with indication, where appropriate, of relevant passages | Relevant to claims | CLASSIFICATION OF THE APPLICATION (Int.Cl.7) |
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| | | | H01Q H04B |
| The present search report has been drawn up for all claims | | | |
| Place of search THE HAGUE | | Date of completion of the search 8 October 2003 | Examiner Van Dooren, G |
| CATEGORY OF CITED DOCUMENTS X: particularly relevant if taken alone Y: particularly relevant if combined with another document of the same category A: technological background O: non-written disclosure P: intermediate document | | T: theory or principle underlying the invention E: earlier patent document, but published on, or after the filing date O: document cited in the application L: document cited for other reasons * : member of the same patent family, corresponding document | |

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ON EUROPEAN PATENT APPLICATION NO.**

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